



**Model Answer
End-Sem Examination-I, Winter 2025**

Academic Year: 2025-2026	Semester: I
Class: FY	Program: BTech
Branch Code: ETC	Pattern: 2023
Name of Course: Electrical Network	Course Code: 2300118E

Q. No.	Answer Details	Max. Marks
Q.1.	<p>Voltage Source to Current Source Conversion An ideal voltage source with a series resistance can be converted into an equivalent current source with a parallel resistance. Voltage Source Representation:</p> <ul style="list-style-type: none">• Voltage Source (V_S): The value of the voltage source.• Series Resistance (R_S): The resistance in series with the voltage source. <p>Current Source Representation:</p> <ul style="list-style-type: none">• Current Source (I_S): The value of the current source.• Parallel Resistance (R_P): The resistance in parallel with the current source. <p>The relationships are: $I_S = \frac{V_S}{R_S}$, $R_P = R_S$</p> <p style="text-align: right;">(3 marks)</p> <p>Current Source to Voltage Source Conversion An ideal current source with a parallel resistance can be converted into an equivalent voltage source with a series resistance. current Source Representation:</p> <ul style="list-style-type: none">• Current Source (I_S): The value of the current source.• Parallel Resistance (R_P): The resistance in parallel with the current source. <p>Voltage Source Representation:</p> <ul style="list-style-type: none">• Voltage Source (V_S): The value of the voltage source.• Series Resistance (R_S): The resistance in series with the voltage source. <p>The relationships are: $V_S = I_S R_P$, $R_S = R_P$</p> <p style="text-align: right;">(3 marks)</p>	[12]
Q.2.		



		<p style="text-align: center;"> Resistor Voltage in phase with current Inductor Voltage leads current by 90° Capacitor Voltage lags current by 90° (2 marks for each phasor diagram) </p>	
Q.3.	A	<p>The Laplace transform is a mathematical tool that is used to convert the differential equation in the time domain into the algebraic equations in the frequency domain or s-domain.</p> <p>Mathematically, if $x(t)$ is a time domain function, then its Laplace transform is defined as –</p> $\mathcal{L}[x(t)] = X(s) = \int_0^{\infty} x(t)e^{-st} dt$ <p>where, s is a complex frequency domain parameter, $s = \sigma + j\omega$, with real numbers $\sigma (>0)$ and ω.</p> <p>The function must satisfy the following condition for its transform to exist:</p> $\int_0^{\infty} x(t) e^{-\sigma t} dt < \infty$ <p style="text-align: right;">(4 marks)</p> <p>. $f(t) = e^{-at}$, or, $e^{-at}u(t)$</p> $\begin{aligned} \mathcal{L}[f(t)] = F(s) &= \int_0^{\infty} e^{-at} \cdot e^{-st} dt = \int_0^{\infty} e^{-(s+a)t} dt = \frac{e^{-(s+a)t}}{-(s+a)} \Big _{t=0}^{t \rightarrow \infty} \\ &= -\frac{1}{(s+a)} \left[(e^{-(s+a)t})_{t \rightarrow \infty} - (e^{-(s+a)t})_{t=0} \right] = \frac{1}{(s+a)} \end{aligned}$ <p style="text-align: right;">(4 marks)</p>	[8]
	B		[8]
		When the switch is closed at $t=0$, current $i(t)$ starts flowing through the resistor	



and inductor. The KVL equation becomes:

$$V = i(t)R + L \frac{di}{dt} \quad (1 \text{ marks})$$

In Laplace domain, this becomes

$V/s = I(s)R + LsI(s)$ as the inductor is relaxed initially.

$$V(s) = I(s)(R + Ls) \quad (1 \text{ marks})$$

$$I(s) = \frac{1}{s} \frac{V}{(R + Ls)} = \frac{1}{s} \frac{V/L}{(R/L + s)} = \frac{A}{s} + \frac{B}{s + \frac{R}{L}}$$

Solving for A and B, we get

$$A = sI(s)|_{s=0} = \frac{V/L}{(s + R/L)} \Big|_{s=0} = \frac{V/L}{R/L} = \frac{V}{R}$$

$$B = (s + R/L)I(s)|_{s=-R/L} = \frac{V/L}{-R/L} = -\frac{V}{R}$$

(4 marks)

$$\text{So, } I(s) = \frac{V/R}{s} + \frac{-V/R}{s + R/L}$$

Taking inverse Laplace, we get

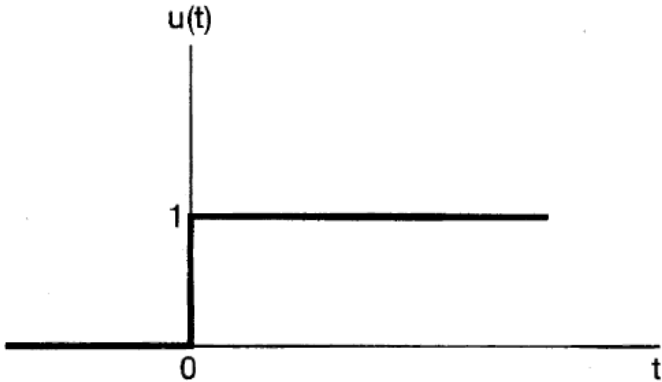
$$i(t) = \frac{V}{R} \left(1 - e^{-\frac{R}{L}t}\right) u(t)$$

(2 marks)

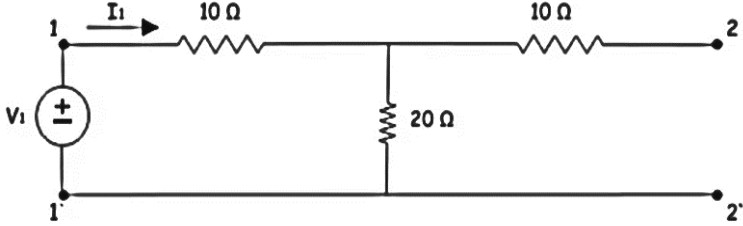
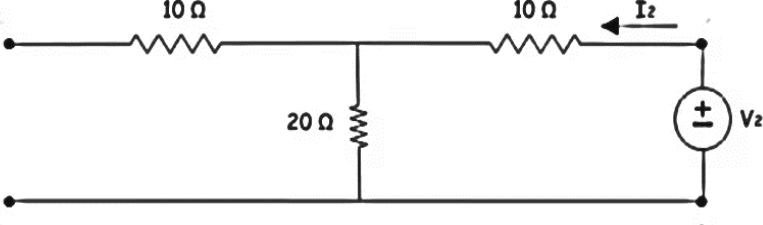


C	$I(s) = \frac{1}{s} \frac{a/b}{(s + c/d)}$ <p>Using partial fraction expansion,</p> $I(s) = \frac{1}{s} \frac{a/b}{(s + c/d)}$ $= \frac{A}{s} + \frac{B}{s + c/d}$ <p style="text-align: right;">(2 marks)</p> <p>Solving for A and B,</p> $sI(s) = A + \frac{Bs}{s + c/d}$ $A = sI(s) _{s=0} = \frac{a/b}{(s + c/d)} \Big _{s=0} = \frac{a/b}{c/d} = \frac{ad}{bc}$ $(s + c/d)I(s) = \frac{A(s + \frac{c}{d})}{s} + B$ $B = (s + c/d)I(s) _{s=-c/d} = \frac{a/b}{-c/d} = \frac{-ad}{bc}$ <p style="text-align: right;">(4 marks)</p> <p>So, $I(s) = \frac{ad}{bc} \frac{1}{s} + \frac{-ad}{bc} \frac{1}{s+c/d}$</p> <p>Taking inverse Laplace, we get</p> $i(t) = \frac{ad}{bc} \left(1 - e^{-\frac{c}{d}t}\right) u(t)$ <p style="text-align: right;">(2 marks)</p>	[8]
D	<p>The unit-step function, denoted by $u(t)$, is a piecewise function that is zero for negative time and one for zero or positive time.</p> <p>The unit-step function is defined as:</p> $u(t) = \begin{cases} 1 & t > 0 \\ 0 & \text{otherwise} \end{cases}$ <p style="text-align: right;">(4 marks)</p>	[8]



		 <p style="text-align: center;">It may be noted that the unit-step is discontinuous at t=0.</p> <p style="text-align: right;">(4 marks)</p> <p>Laplace Transform of the Unit-Step Function The Laplace transform of the unit-step function can be found using the definition of the Laplace transform:</p> $\mathcal{L}[u(t)] = \int_0^{\infty} u(t)e^{-st} dt = \int_0^{\infty} e^{-st} dt = \frac{e^{-st}}{-s} \Big _0^{\infty} = 0 - \left(-\frac{1}{s}\right) = \frac{1}{s}$ <p style="text-align: right;">(4 marks)</p>	
Q.4.	A	<p>The short-circuit admittance parameters, also known as Y-parameters, are used to describe the electrical behavior of linear two-port networks using admittance (the inverse of impedance). These parameters are particularly useful when dealing with high-frequency circuits and can be measured when all ports are short-circuited except the one where the measurement is taken.</p> <p style="text-align: right;">(2 marks)</p> <p>For a two-port network with input port (1) and output port (2), the Y-parameters are defined as follows:</p> <ul style="list-style-type: none"> • y_{11}: Input admittance with output port short-circuited. • y_{12}: Reverse transfer admittance with input port short-circuited. • y_{21}: Forward transfer admittance with output port short-circuited. • y_{22}: Output admittance with input port short-circuited. <p style="text-align: right;">(2 marks)</p> <p>Currents I_1 and I_2 are related to voltages V_1 and V_2 as:</p> $I_1 = y_{11}V_1 + y_{12}V_2$ $I_2 = y_{21}V_1 + y_{22}V_2$ <p>Which is represented in matrix form as:</p> $\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$ <p style="text-align: right;">(4 marks)</p>	[8]



B	<p>Steps for z-parameters :</p> <p>1. Connect a supply V_1 at port 1, to make a current I_1 flow at port 1-1'</p>  <p>This gives,</p> $I_1 = \frac{V_1}{30}, \quad V_2 = 20I_1$ $z_{11} = \left(\frac{V_1}{I_1} \mid I_2 = 0 \right) = 30 \Omega$ $z_{21} = \left(\frac{V_2}{I_1} \mid I_2 = 0 \right) = 20 \Omega$ <p>2. Connect a supply V_2 at port 2, to make a current I_2 flow at port 2-2'.</p>  $I_2 = \frac{V_2}{30}, \quad V_1 = 20I_2$ $z_{12} = \left(\frac{V_1}{I_2} \mid I_1 = 0 \right) = 20 \Omega$ $z_{22} = \left(\frac{V_2}{I_2} \mid I_1 = 0 \right) = 30 \Omega$ <p style="text-align: right;">(4 marks)</p> <p>Now convert z-parameters to y-parameters as</p> $\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} \frac{z_{22}}{z_{11}z_{22} - z_{12}z_{21}} & \frac{-z_{12}}{z_{11}z_{22} - z_{12}z_{21}} \\ \frac{-z_{21}}{z_{11}z_{22} - z_{12}z_{21}} & \frac{z_{11}}{z_{11}z_{22} - z_{12}z_{21}} \end{bmatrix}$ $\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} \frac{30}{900 - 400} & \frac{-20}{900 - 400} \\ \frac{-20}{900 - 400} & \frac{30}{900 - 400} \end{bmatrix}$ $\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} 0.06 & -0.04 \\ -0.04 & 0.06 \end{bmatrix} \Omega^{-1}$ <p style="text-align: right;">(4 marks)</p>	[8]
C	<p>Hybrid parameters, or h-parameters, are used to describe the behavior of linear two-port networks, often in transistor modeling and small-signal analysis. The term "hybrid" comes from the fact that these parameters are a mix of impedance, admittance, and dimensionless ratios, making them versatile for various applications.</p>	[8]



The h-parameters are defined as follows:

- h_{11} : Input impedance with output port short-circuited
- h_{12} : Reverse voltage gain with input port open-circuited
- h_{21} : Forward current gain with output port short-circuited
- h_{22} : Output admittance with input port open-circuited

The relationship between the voltages and currents in terms of h-parameters is given by:

$$V_1 = h_{11}I_1 + h_{12}V_2, \quad I_2 = h_{21}I_1 + h_{22}V_2$$

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

(4 marks)

where:

- h_{11} : Input impedance with output short-circuited ($V_2 = 0$).

$$h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0}$$

- h_{12} : Reverse voltage gain with input open-circuited ($I_1 = 0$).

$$h_{12} = \left. \frac{V_1}{V_2} \right|_{I_1=0}$$

- h_{21} : Forward current gain with output short-circuited ($V_2 = 0$).

$$h_{21} = \left. \frac{I_2}{I_1} \right|_{V_2=0}$$

- h_{22} : Output admittance with input open-circuited ($I_1 = 0$).

$$h_{22} = \left. \frac{I_2}{V_2} \right|_{I_1=0}$$

(4 marks)



D	$Z = \begin{bmatrix} 1 & 2 \\ 3 & 4 \end{bmatrix}$ $\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} \frac{Z_{22}}{Z_{11}Z_{22} - Z_{12}Z_{21}} & \frac{-Z_{12}}{Z_{11}Z_{22} - Z_{12}Z_{21}} \\ \frac{-Z_{21}}{Z_{11}Z_{22} - Z_{12}Z_{21}} & \frac{Z_{11}}{Z_{11}Z_{22} - Z_{12}Z_{21}} \end{bmatrix}$ $\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} \frac{4}{1 * 4 - 2 * 3} & \frac{-2}{1 * 4 - 2 * 3} \\ \frac{-3}{1 * 4 - 2 * 3} & \frac{1}{1 * 4 - 2 * 3} \end{bmatrix}$ $= \begin{bmatrix} 4 & -2 \\ -2 & -2 \\ -3 & 1 \\ -2 & -2 \end{bmatrix} = \begin{bmatrix} -2 & 1 \\ 1.5 & 0.5 \end{bmatrix} \Omega^{-1}$	[8]
Q.5	<p style="text-align: center;"><u>Star to Delta Transformation</u></p> <div style="text-align: center;"> </div> $R_{12} = R_1 + R_2 + \frac{R_1 R_2}{R_3}$ $R_{13} = R_1 + R_3 + \frac{R_1 R_3}{R_2}$ $R_{23} = R_2 + R_3 + \frac{R_2 R_3}{R_1}$ <p style="text-align: right;">(2 marks for figure) (2 marks for each equation)</p>	[8]



B	<div style="text-align: center;"> </div> <p>Average Value = Area under one cycle = $v_{avg} = \frac{1}{2\pi} \int_0^{2\pi} v d(\omega t) = 0$</p> <p>RMS or Effective Value = $v_{rms} = \sqrt{\frac{1}{2\pi} \int_0^{2\pi} v^2 d(\omega t)} = \frac{A_{peak}}{\sqrt{2}}$</p> <p style="text-align: right;">(2 marks for figure) (3 marks for each equation)</p>	[8]
C	<p>The impulse function, often denoted by $\delta(t)$, is a mathematical function with unique properties that make it useful in signal processing, control systems, and communications. The impulse function, also known as the Dirac delta function, is not a traditional function but rather a generalized function or "distribution" that is used to model an idealized instantaneous impulse.</p> <p>Definition of Impulse Function</p> <p>The impulse function $\delta(t)$ is defined by the following properties:</p> <ol style="list-style-type: none"> 1. It is zero everywhere except at $t = 0$. 2. The area under $\delta(t)$ is equal to 1, i.e., $\int_{-\infty}^{\infty} \delta(t) dt = 1$ <ol style="list-style-type: none"> 3. It represents an infinitely high, infinitely narrow spike at $t = 0$, with an area of 1, which is useful for modeling instantaneous events. <p>In practical terms, the impulse function is often used to "sample" a value of another function at a specific point in time, which is fundamental in systems analysis.</p> <p style="text-align: right;">(4 marks)</p> <p style="text-align: center;">Important properties of $\delta(t)$:</p> <ol style="list-style-type: none"> 1. $\int_{-\infty}^{\infty} \delta(t) dt = 1$ 2. Total area under $\delta(t) = 1$ 3. The function has zero value everywhere els 4. $\int_{-\infty}^{\infty} f(t)\delta(t) dt = f(0)$ 5. $\int_{-\infty}^{\infty} f(t)\delta(t - a) dt = f(a)$ <p style="text-align: right;">Total (4 marks)</p>	



D	<div style="text-align: center;"> <p>OR</p> </div> <p>Steps :</p> <ol style="list-style-type: none"> 1. Connect a supply V_1 at port 1, to make a current I_1 flow at port 1. 2. The total resistance of the circuit R, seen from port 1 will be the parallel combination of resistance 4 ohm and two series resistances of 8 ohms each. Thus $R = 4 \parallel 16 = 16/5$ ohms. 3. Also, the current division rule gives the current through resistance 16 ohm as $I = \frac{4}{16+4} I_1 = \frac{1}{5} I_1$ A. This gives voltage across 8-ohm resistance V_2 as $V_2 = 8 * \frac{1}{5} I_1 = \frac{8}{5} I_1$. <p>This gives,</p> $z_{11} = \left(\frac{V_1}{I_1} \mid I_2 = 0 \right) = 16/5 \Omega$ $z_{21} = \left(\frac{V_2}{I_1} \mid I_2 = 0 \right) = 8/5 \Omega$ <p style="text-align: right;">(4 marks)</p> <ol style="list-style-type: none"> 4. Connect a supply V_2 at port 2, to make a current I_2 flow at port 2 5. The total resistance of the circuit R, seen from port 2 will be the parallel combination of resistance 8 ohm and two resistances in series of 8 ohm and 4 ohm (=12 ohm). Thus $R = 8 \parallel 12 = 24/5$ ohms. 6. Also, the current division rule gives the current through resistance 8 ohm as $I = \frac{12}{12+8} I_2 = \frac{12}{20} I_2 = \frac{3}{5} I_2$ A. This gives voltage across 8-ohm resistance V_1 as $V_1 = 8 * \frac{3}{5} I_2 = \frac{24}{5} I_2$. $z_{12} = \left(\frac{V_1}{I_2} \mid I_1 = 0 \right) = 24/5 \Omega$ $z_{22} = \left(\frac{V_2}{I_2} \mid I_1 = 0 \right) = 8/5 \Omega$ <p style="text-align: right;">(4 marks)</p>	
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